

Solution by Michael Zakoworotny

4) Pendulum. A uniform block (width = w , height = h , mass = m) is suspended by two massless rigid rods AB and CD with lengths L that have ideal bearings at their ends (A, B, C & D). Gravity g causes the pendulum to swing. The pendulum is released from rest (all velocities at $t = 0$ are $\vec{0}$) at $\theta = \theta_0$.

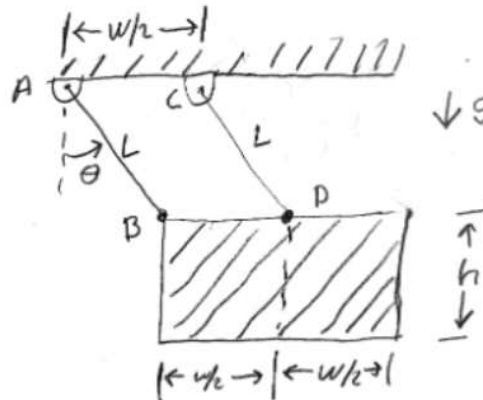
* All answers below should be in terms of some or all of w, h, m, L, g and θ_0 .

* Hint: all points on the block have the same acceleration.

a) Immediately after release, find tension AB or CD (your choice)?

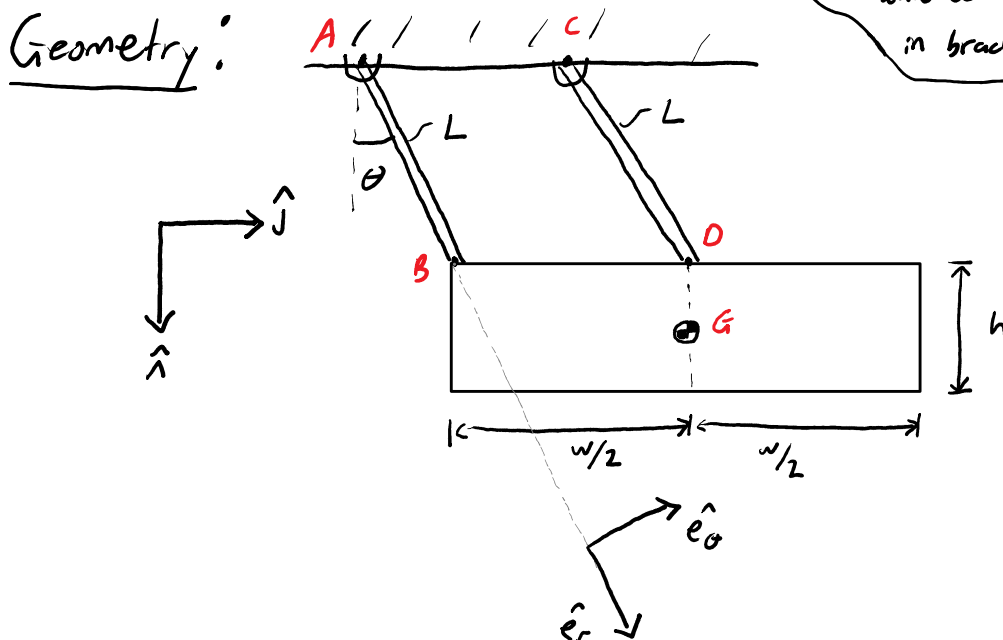
b) Find the equations of motion (e.g., find differential equations that, if you solved them would give you the motion.)

c) Find tensions AB and CD (both of them) when the pendulum has swung down to $\theta = 0$.

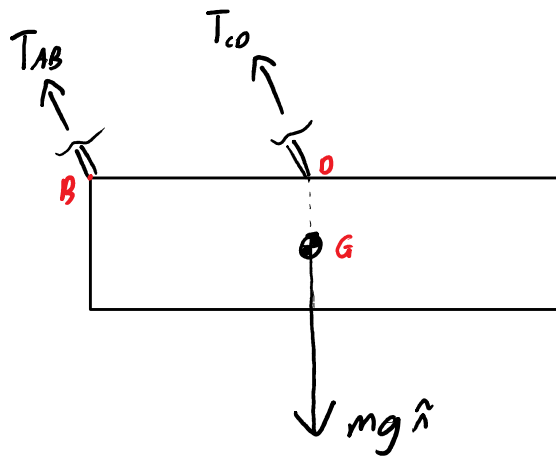


Given: L, w, h, m, g
 $\theta(0) = \theta_0, \dot{\theta}(0) = 0$

Note: Solution is more thorough than what is expected on exam. Full credit can be achieved w/o including items in brackets []



FBD



The block only moves translationally because it is constrained to never rotate about its C.G. Therefore, the velocity and acceleration of all points on the block are equal: $\vec{a}_B = \vec{a}_O = \vec{a}_G$

a) Find T_{AB} or T_{CO} at $t=0$

Let: $\hat{e}_r = \cos\theta \hat{i} + \sin\theta \hat{j}$
 $\hat{e}_\theta = -\sin\theta \hat{i} + \cos\theta \hat{j}$

LMB: $\sum \vec{F} = m \vec{a}_{G/F} = m \vec{a}_{B/F}$

$$\vec{a}_{B/F} = -L\ddot{\theta}^2 \hat{e}_r + L\ddot{\theta} \hat{e}_\theta$$

$$-T_{AB} \hat{e}_r - T_{CO} \hat{e}_r + mg \hat{i} = m (-L\ddot{\theta}^2 \hat{e}_r + L\ddot{\theta} \hat{e}_\theta) \quad (1)$$

$$\begin{aligned}
 (1) \cdot \hat{e}_\theta: \quad \cancel{mg} \hat{\lambda} \cdot \hat{e}_\theta &= \cancel{mL} \ddot{\theta} & \hat{\lambda} \cdot \hat{e}_\theta &= -\sin \theta \\
 -g \sin \theta &= L \ddot{\theta} & \text{At } t=0, \theta &= \theta_0 \\
 \ddot{\theta} &= -\frac{g}{L} \sin \theta_0 \quad (2)
 \end{aligned}$$

$$\begin{aligned}
 \underline{AMB:} \quad \sum \vec{M}_{i/D} &= \dot{\vec{H}}_{i/D} \\
 &= \int \vec{r}_{i/D} \times \vec{a} \, dm \\
 &\quad \hookrightarrow = a_{G/F}, \text{ constant for all pts on block} \\
 &= \int \vec{r}_{i/D} \, dm \times \vec{a}_{G/F}
 \end{aligned}$$

$$\sum \vec{M}_{i/D} = \vec{r}_{G/D} m_{\text{tot}} \times \vec{a}_{G/F} = \vec{0}, \text{ parallel}$$

$$\begin{aligned}
 \vec{r}_{B/D} \times -T_{AB} \hat{e}_r + \vec{r}_{D/D} \times -T_{CD} \hat{e}_r + \vec{r}_{G/D} \times mg \hat{\lambda} &= \vec{r}_{G/D} \times m \vec{a}_{G/F} \\
 -\frac{w}{2} \hat{j} \times -T_{AB} \hat{e}_r &= \frac{h}{2} \hat{\lambda} \times m (-L \ddot{\theta}^2 \hat{e}_r + L \ddot{\theta} \hat{e}_\theta) \\
 &\quad \hookrightarrow \text{At } t=0, \dot{\theta}=0
 \end{aligned}$$

$$\left\{ -\frac{w}{2} T_{AB} \cancel{\cos \theta_0} \hat{k} = m \frac{h}{2} L \ddot{\theta} \cancel{\cos \theta_0} \hat{k} \right\}$$

$$\{\} \cdot \hat{k}: -w T_{AB} = m h L \ddot{\theta} \leftarrow \text{Apply (2)}$$

$$-w T_{AB} = m h \cancel{L} \cdot -\frac{g}{\cancel{L}} \sin \theta_0$$

$$\boxed{T_{AB} = \frac{m g h}{w} \sin \theta_0} \quad (3)$$

T_{c0} can be found by instead performing AMB about B ... or] by plugging (3) into (1) $\cdot \hat{e}_r$

$$(1) \cdot \hat{e}_r: -T_{AB} - T_{c0} + mg \cos \theta_0 = -mL \ddot{\theta}_0^2$$

$$T_{c0} = mg \cos \theta_0 - \frac{mgh}{w} \sin \theta_0$$

$$T_{c0} = mg \left[\cos \theta_0 - \frac{h}{w} \sin \theta_0 \right]$$

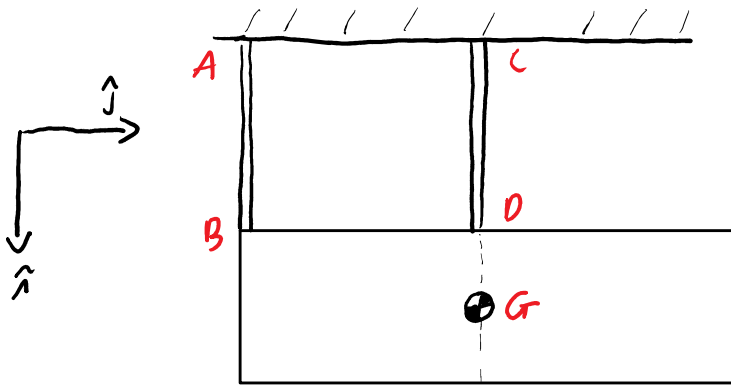
b) Obtain the EOM:
Consider equation (1), from LMB

$$-T_{AB} \hat{e}_r - T_{c0} \hat{e}_r + mg \hat{n} = m(-L \ddot{\theta}^2 \hat{e}_r + L \ddot{\theta} \hat{e}_\theta) \quad (1)$$

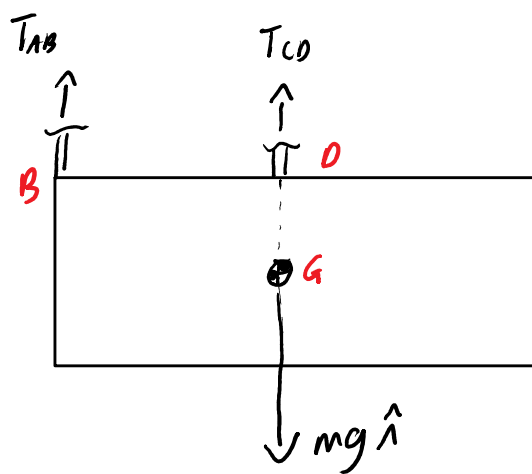
$$\text{Again, } (1) \cdot \hat{e}_\theta: -mg \sin \theta = mL \ddot{\theta}$$

$$\ddot{\theta} = -\frac{g}{L} \sin \theta$$

c) Find both T_{AB} and T_{CD} when $\theta = 0$ (bottom)



At $\theta = 0$, $\hat{e}_r = \hat{i}$, $\hat{e}_\theta = \hat{j}$



In this configuration, G is aligned with rod CD. Rod AB must carry no load, since the block cannot experience any angular accelerations about its C.G.

$$\vec{M}_{/G} = \vec{H}_{/G} = \vec{0} \Rightarrow T_{AB} = 0$$

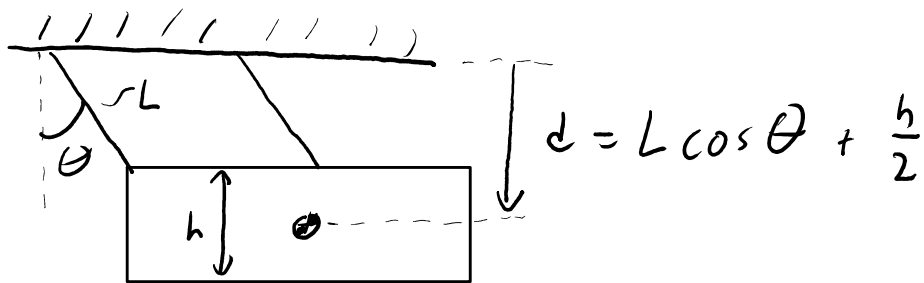
LMB: $\sum \vec{F} = m \vec{a}_{G/J}$

$$\left\{ -T_{CD} \hat{i} + mg \hat{i} = m(-L\dot{\theta}^2 \hat{i} + L\ddot{\theta} \hat{j}) \right\}$$

$$\{ \} \cdot \hat{i}: -T_{CD} + mg = -mL\dot{\theta}^2$$

$$T_{CD} = mg + mL\dot{\theta}^2, \text{ at } \theta = 0 \quad (4)$$

Get $\dot{\theta}^2$ from energy conservation



$$\begin{aligned} \text{At } t=0: E_0 &= -mgd_0 \\ &= -mg(L\cos\theta_0 + \frac{h}{2}) \end{aligned}$$

$$\begin{aligned} \text{At bottom: } E &= -mgd + \frac{1}{2}m|\vec{v}_A|^2 \\ &\quad \downarrow \quad \quad \quad \hookrightarrow |\vec{v}_A| = |\vec{v}_B| \\ d &= L + \frac{h}{2} \text{ at } \theta=0 \quad \quad \quad = L\dot{\theta} \end{aligned}$$

$$E = -mg(L + \frac{h}{2}) + \frac{1}{2}mL^2\dot{\theta}^2$$

Conservation: $E_0 = E$

$$-mg(L\cos\theta_0 + \frac{h}{2}) = -mg(L + \frac{h}{2}) + \frac{1}{2}mL^2\dot{\theta}^2$$

$$\frac{1}{2}L^2\dot{\theta}^2 = gL(1 - \cos\theta_0)$$

$$\dot{\theta}^2 = \frac{2g}{L}(1 - \cos\theta_0) \quad (5)$$

Apply (5) to (4):

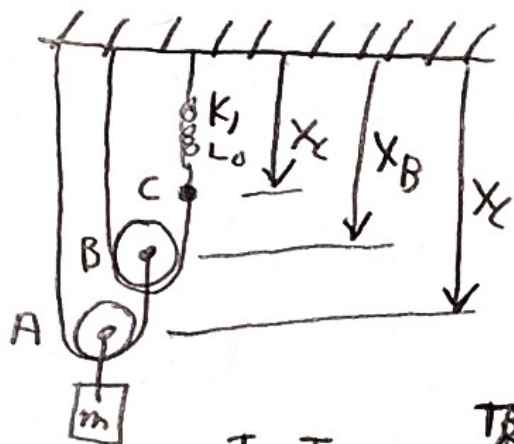
$$T_{co} = mg + m \cancel{L} \cdot \frac{2g}{\cancel{L}} (1 - \cos \theta_0)$$

$$T_{co} = mg(3 - 2 \cos \theta_0), \quad T_{AB} = 0$$

Note: If $\theta_0 = \pi/2$, this results in $T_{co} = 3mg$, which is the same as the particle mass pendulum from lecture.

(5)

Neglect pulley radii & masses,



FBDS:



$$\uparrow T_s = K(x_C - L_0)$$

s = spring stretch

$$\downarrow T_s = T_B$$

Kinematics

String 1: $L_A = x_A + (x_A - x_B)$ (1)

String 2: $L_B = x_B + x_B - x_C$ (2)

Spring: $s = x_C - L_0$ (spring stretch)

LMB: $m\ddot{x}_A = \sum F$ (3)

$= mg - 2T_A$ (FBD A)

$\uparrow T_A = 2T_B$ (FBD B)

$\uparrow T_B = T_s$ (FBD spring)

$\uparrow T_s = k(x_C - L_0)$

(2) $\Rightarrow x_C = 2x_B - L_B$

(1) $\Rightarrow x_B = 2x_A - L_A$

Back substitute through relations above

(5) $\rightarrow X_C = 2X_B - L_B = 4X_A - 2L_A - L_B$ 2/3

$$T_S = K(X_C - L_0) = K(4X_A - (\underbrace{2L_A + L_B + L_0}_{\equiv L})) \quad (4)$$

$$T_A = 2T_B = 2T_S = 2K(4X_A - L)$$

LMB (again)

$$(3) \quad m\ddot{X}_A = mg - 2T_A$$

$$= mg - 16KX_A + 4LK$$

$$\Rightarrow \boxed{m\ddot{X}_A + 16KX = mg + 4LK}$$

$$\boxed{\omega = \sqrt{16K/m} = 4\sqrt{K/m}} \quad (a)$$

problem statement

(b)

$$X_A = X_p + X_h$$

$$\quad \quad \quad \uparrow \quad \quad \quad \nearrow 0 \quad \quad \quad \nearrow d$$

$$\quad \quad \quad \uparrow \quad \quad \quad A \cos(\omega t) + B \sin(\omega t)$$

$$X_p = \frac{mg}{16K} + L/4$$

(5)

Want $T_S > 0$. At extreme $T_S = 0$.

$$\quad \quad \quad \uparrow \quad \quad \quad \uparrow \quad \quad \quad X_A = X_p = d$$

$$\quad \quad \quad \uparrow \quad \quad \quad \uparrow \quad \quad \quad \text{most up}$$

$$T_S = 0 \text{ \& (4) } \Rightarrow 4X_A - L = 0$$

$$\Rightarrow 4X_p - 4d - L = 0$$

$$(5) \Rightarrow \left(\frac{mg}{4K} + L\right) - 4d - L = 0$$

\Rightarrow biggest possible

$$\boxed{d = mg/16K}$$

(5)

3/3

(b) Intuitive Solution :

max amplitude = d = displacement of mass
due to gravity

(starting w/ no slack)

[At that displacement there is no
slack & no tension, Any more and
there will be slack]

$$\underbrace{\text{stretch of spring}}_{\text{statics}} = \frac{\text{spring tension}}{K}$$

$$= \frac{mg/4}{K}$$

$$= mg/4K$$

$$\text{Displacement of mass} = (\text{spring stretch})/4$$

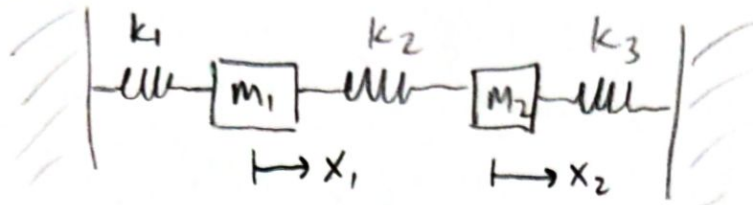
↑ 2 pulleys

\Rightarrow

$$d = \frac{mg}{16K} = \text{static disp. of A due to gravity}$$

P6: Vibrations

GIVEN:



→ all springs relaxed in equilibrium position as pictured

PART A: find governing equations, write in matrix form

FBD's:
~~~~~



From this we receive EOM's:

$$① \quad m_1 \ddot{x}_1 = k_2 x_2 - (k_1 + k_2) x_1$$

$$② \quad m_2 \ddot{x}_2 = -(k_2 + k_3) x_2 + k_2 x_1$$

put into matrix:

$$M \ddot{x} + \cancel{C} \dot{x} + Kx = \cancel{F}$$

no damping      no forcing

$$\begin{bmatrix} m_1 & 0 \\ 0 & m_2 \end{bmatrix} \begin{bmatrix} \ddot{x}_1 \\ \ddot{x}_2 \end{bmatrix} + \begin{bmatrix} (k_1 + k_2) & -k_2 \\ -k_2 & (k_2 + k_3) \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} = 0$$

M                       $\ddot{x}$                       K                      x

PART B: Given  $k_2 = k_1$ ,  $k_3 = 4k_1$ ,  $M_2 = 2m_1$ ,

Determine if  $\begin{bmatrix} x_1 \\ x_2 \end{bmatrix} = \sin(\lambda t) \begin{bmatrix} 1 \\ -1 \end{bmatrix}$

is a normal mode.

★ translation: is  $\sin(\lambda t) \begin{bmatrix} 1 \\ -1 \end{bmatrix}$  a solution  
to our EOM?

EOM: ①  $M_1 \ddot{x}_1 = -(k_1 + k_2)x_1 + k_2 x_2$

②  $M_2 \ddot{x}_2 = k_2 x_1 - (k_2 + k_3)x_2$

plug  
in

$x_1 = \sin \lambda t$

$\ddot{x}_1 = -\lambda^2 \sin \lambda t$

$x_2 = -\sin \lambda t$

$\ddot{x}_2 = \lambda^2 \sin \lambda t$

①  $m_1 (\cancel{\lambda^2 \sin \lambda t}) = -(k_1 + k_2)(\cancel{\sin \lambda t}) - k_2 \cancel{\sin \lambda t}$

$-m_1 \lambda^2 = -(k_1 + k_2) - k_2$

plug in params:

$-m_1 \lambda^2 = -2k_1 - k_1 = -3k_1$

$\lambda^2 = 3k_1 / m_1$

②  $m_2 (\cancel{\lambda^2 \sin \lambda t}) = k_2 (\cancel{\sin \lambda t}) - (k_2 + k_3)(\cancel{-\sin \lambda t})$

$m_2 \lambda^2 = k_2 + (k_2 + k_3)$

plug in params:

$2m_1 \lambda^2 = 2k_1 + 4k_1 = 6k_1$

$\lambda^2 = 6k_1 / 2m_1 = 3k_1 / m_1$

both equations ① & ② are satisfied if  $\lambda = \sqrt{3k_1 / m_1}$ , which  
means that the solution we tried ( $\begin{bmatrix} x_1 \\ x_2 \end{bmatrix} = \sin(\lambda t) \begin{bmatrix} 1 \\ -1 \end{bmatrix}$ )  
is a TRUE solution. so YES, the person  
is right. 😊



# ★ ★ 2 extra methods for Part B: eigenvectors ★

PART B: Given  $k_2 = k_1$ ,  $k_3 = 4k_1$ ,  $m_2 = 2m_1$ ,

Determine if  $\begin{bmatrix} x_1 \\ x_2 \end{bmatrix} = \sin(\lambda t) \begin{bmatrix} 1 \\ -1 \end{bmatrix}$  is a normal mode.

★ alternative translation: is  $\begin{bmatrix} 1 \\ -1 \end{bmatrix}$  an eigenvector of  $\underbrace{[M \setminus K]}_{\text{"A"}}$ ?

first compute A matrix:

$$A = M \setminus K = M^{-1} K = \begin{bmatrix} (k_1 + k_2)/m_1 & -k_2/m_1 \\ -k_2/m_2 & (k_2 + k_3)/m_2 \end{bmatrix}$$

setting  $k_1 = 1 \dots m_1 = 1 \dots$

$\hookrightarrow k_2 = 1 \quad \hookrightarrow m_2 = 2$   
 $k_3 = 4$

then A becomes:

↑  
TBH could have left it all symbolic but I didn't want to

$$\begin{bmatrix} (1+1)/1 & -1/1 \\ -1/2 & (1+4)/2 \end{bmatrix} = \begin{bmatrix} 2 & -1 \\ -1/2 & 5/2 \end{bmatrix}$$

Q: is  $\begin{bmatrix} 1 \\ -1 \end{bmatrix}$  an eigenvector of  $\begin{bmatrix} 2 & -1 \\ -1/2 & 5/2 \end{bmatrix}$ ?

1 eigenvector check method:

if  $A \begin{bmatrix} 1 \\ -1 \end{bmatrix} = S \begin{bmatrix} 1 \\ -1 \end{bmatrix}$ , then  $\begin{bmatrix} 1 \\ -1 \end{bmatrix}$  is an eigenvector (& normal mode)  
↑ any scalar

compute:

$$\begin{bmatrix} 2 & -1 \\ -1/2 & 5/2 \end{bmatrix} \begin{bmatrix} 1 \\ -1 \end{bmatrix} = \begin{bmatrix} 2-1 \\ -1/2 - 5/2 \end{bmatrix} = \begin{bmatrix} 1 \\ -3 \end{bmatrix} = \checkmark S \begin{bmatrix} 1 \\ -1 \end{bmatrix}$$

yes,  $\begin{bmatrix} 1 \\ -1 \end{bmatrix}$  works as a normal mode :)

2 Marigot's "I hate eigenvectors but love MATLAB" method:

MATLAB:

$$A = \begin{bmatrix} -2 & 1 \\ 1/2 & -5/2 \end{bmatrix}$$

$$[vec, val] = eig(A)$$

$$vec1 = vec(:, 1)$$

$$vec2 = vec(:, 2)$$

$$mode = [-1; 1]$$

$$s1 = vec1 ./ mode$$

$$s2 = vec2 ./ mode$$

if  $s1(1) == s1(2)$

disp('yes')

elseif  $s2(1) == s2(2)$

disp('yes')

else

disp('no')

← I know [vec] will have the normalized eigenvectors

← unpack [vec] into the separate eigenvectors

← mode that we're hoping either [vec1] or [vec2] is a multiple of

← [s1] & [s2] will be vectors

← if the elements in [s1] are the same, [vec1] is a scalar multiple of [mode]

← same for [s2] and [vec2]

← if neither [vec1] nor [vec2] is a scalar multiple of [mode]... we will get 'no.'

(this will end up printing... which you wouldn't necessarily know on the test. that's OK! Nearly full points for code that will give the right answer when run.)